

# Nomogram to calculate oxygen consumption

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**SUMMARY** A nomogram has been devised for the rapid derivation of the oxygen consumption from the expired minute volume and the fractional concentrations of expired CO<sub>2</sub> and O<sub>2</sub>.

The oxygen consumption is a prerequisite for determining the cardiac output by the Fick method. It is obtained after breathing room air for a known period of time, by measuring the minute volume, and the fractional concentrations of carbon dioxide, and oxygen of the expired air.

As the calculation of the oxygen consumption is a tedious one to perform, a nomogram has been devised to help. The nomogram may also be useful in cross-checking rapidly a large number of calculations.

## Theory

Oxygen consumption = volume of inspired - volume of expired oxygen, or

$$\dot{V}O_2 = \dot{V}_I \times F_{I O_2} - \dot{V}_E \times F_{E O_2} \dots \dots (1)$$

where  $\dot{V}O_2$  = oxygen consumption (l/min)  
 $\dot{V}_I$  = inspired volume of air (l/min)  
 $F_{I O_2}$  = fractional concentration of inspired O<sub>2</sub> = 0.2093  
 $\dot{V}_E$  = expiratory minute volume of air (l/min) measured at ATPS  
 $F_{E O_2}$  = fractional concentration of expired O<sub>2</sub>.

Since, in a steady state the body neither produces nor consumes nitrogen, inspired volume of nitrogen = expired volume of nitrogen, or

$$\dot{V}_I \times F_{I N_2} = \dot{V}_E \times F_{E N_2} \dots \dots \dots (2)$$

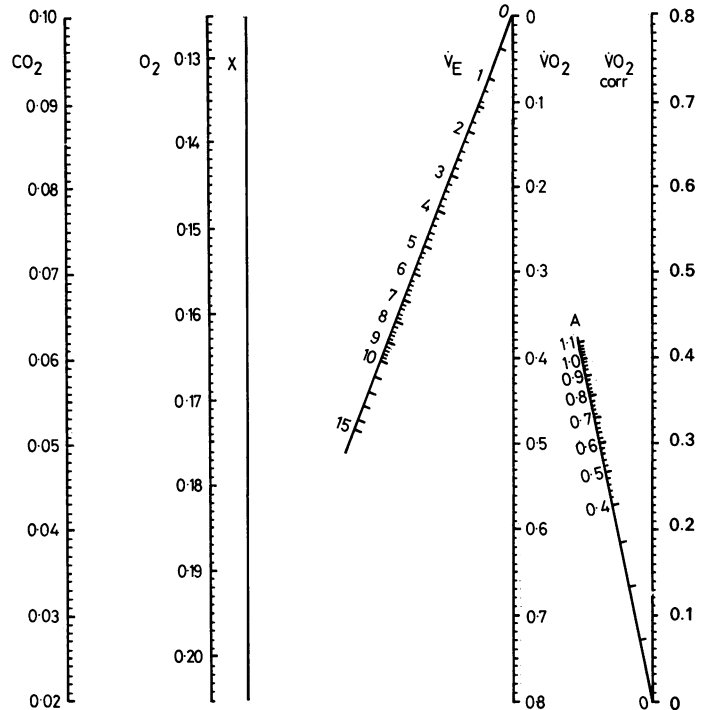
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**Table** Conversion factors to reduce saturated gas volume at ambient temperature and pressure to STPD

| $\frac{P}{T_{oc}}$ mmHg | 700   | 705   | 710   | 715   | 720   | 725   | 730   | 735   | 740   | 745   | 750   |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 15                      | 0.857 | 0.863 | 0.870 | 0.876 | 0.882 | 0.888 | 0.895 | 0.900 | 0.907 | 0.913 | 0.919 |
| 16                      | 0.853 | 0.859 | 0.866 | 0.872 | 0.880 | 0.884 | 0.890 | 0.897 | 0.903 | 0.909 | 0.915 |
| 17                      | 0.849 | 0.855 | 0.861 | 0.868 | 0.874 | 0.880 | 0.886 | 0.892 | 0.899 | 0.905 | 0.911 |
| 18                      | 0.845 | 0.851 | 0.857 | 0.863 | 0.870 | 0.876 | 0.882 | 0.888 | 0.894 | 0.900 | 0.907 |
| 19                      | 0.841 | 0.847 | 0.853 | 0.859 | 0.865 | 0.872 | 0.877 | 0.884 | 0.890 | 0.896 | 0.902 |
| 20                      | 0.837 | 0.843 | 0.849 | 0.855 | 0.861 | 0.867 | 0.873 | 0.880 | 0.886 | 0.891 | 0.900 |
| 21                      | 0.832 | 0.839 | 0.845 | 0.851 | 0.857 | 0.863 | 0.869 | 0.875 | 0.881 | 0.887 | 0.893 |
| 22                      | 0.828 | 0.834 | 0.840 | 0.846 | 0.853 | 0.859 | 0.865 | 0.871 | 0.877 | 0.883 | 0.889 |
| 23                      | 0.824 | 0.830 | 0.836 | 0.842 | 0.848 | 0.854 | 0.860 | 0.866 | 0.872 | 0.878 | 0.885 |
| 24                      | 0.819 | 0.826 | 0.832 | 0.838 | 0.844 | 0.850 | 0.856 | 0.862 | 0.868 | 0.874 | 0.880 |
| 25                      | 0.815 | 0.821 | 0.827 | 0.833 | 0.839 | 0.845 | 0.851 | 0.857 | 0.863 | 0.869 | 0.875 |
| 26                      | 0.811 | 0.817 | 0.823 | 0.829 | 0.835 | 0.841 | 0.847 | 0.853 | 0.859 | 0.865 | 0.871 |
| 27                      | 0.806 | 0.812 | 0.818 | 0.824 | 0.830 | 0.836 | 0.842 | 0.848 | 0.854 | 0.860 | 0.866 |
| 28                      | 0.801 | 0.807 | 0.813 | 0.819 | 0.825 | 0.831 | 0.837 | 0.843 | 0.849 | 0.855 | 0.861 |

**Fig. 1** Nomogram for estimation of oxygen consumption.  $\text{CO}_2$ , fractional concentration of expired  $\text{CO}_2$ ;  $\text{O}_2$ , fractional concentration of expired  $\text{O}_2$ ;  $V_E$ , expired minute volume l/min ATPS;  $V_{\text{O}_2}$ , computed  $\text{O}_2$  consumption l/min;  $V_{\text{O}_2 \text{ corr}}$ , corrected  $\text{O}_2$  consumption l/min;  $A$ , adjustment factor.

A straight line joining  $\text{CO}_2$  and  $\text{O}_2$  intersects the unscaled line  $x$ . A second straight line drawn between the point on  $x$  and  $V_E$  is extended to  $V_{\text{O}_2}$ . A third straight line is then drawn between the point on  $V_{\text{O}_2}$  and  $A$  to intersect  $V_{\text{O}_2 \text{ corr}}$  to obtain corrected oxygen consumption.



where the fractional concentration of inspired nitrogen ( $F_{\text{I N}_2}$ ) =  $1 - F_{\text{I O}_2} - F_{\text{I CO}_2}$  =  $1 - 0.2093 - 0$  or  $0.7907$ , as fractional concentration of inspired carbon dioxide ( $F_{\text{I CO}_2}$ ) is considered to be negligible.  $F_{\text{E N}_2}$  is the fractional concentration of expired nitrogen =  $1 - F_{\text{E CO}_2} - F_{\text{E O}_2}$ , where  $F_{\text{E CO}_2}$  is the fractional concentration of expired carbon dioxide; or

$$\dot{V}_{\text{I}} = \frac{\dot{V}_{\text{E}} (1 - F_{\text{E CO}_2} - F_{\text{E O}_2})}{0.7907} \quad \dots (3)$$

Substituting for  $\dot{V}_{\text{I}}$  in equation (1) from equation (3) we get:

$$\dot{V}_{\text{O}_2} = \left[ \frac{\dot{V}_{\text{E}} (1 - F_{\text{E CO}_2} - F_{\text{E O}_2})}{0.7907} \times F_{\text{I O}_2} \right] - \left[ \dot{V}_{\text{E}} \times F_{\text{E O}_2} \right]$$

as  $F_{\text{I O}_2}$  =  $0.2093$  we get on simplification:

$$\dot{V}_{\text{O}_2} = (0.265 \times \dot{V}_{\text{E}}) - (1.265 \times \dot{V}_{\text{E}} \times F_{\text{E O}_2}) - (0.265 \times \dot{V}_{\text{E}} \times F_{\text{E CO}_2}) \quad \dots (4)$$

| 755   | 760   | 765   | 770   | 775   | 780   |
|-------|-------|-------|-------|-------|-------|
| 0.926 | 0.932 | 0.938 | 0.944 | 0.951 | 0.957 |
| 0.921 | 0.928 | 0.934 | 0.940 | 0.946 | 0.952 |
| 0.917 | 0.923 | 0.930 | 0.936 | 0.942 | 0.948 |
| 0.913 | 0.919 | 0.925 | 0.931 | 0.937 | 0.944 |
| 0.908 | 0.915 | 0.921 | 0.927 | 0.933 | 0.939 |
| 0.904 | 0.910 | 0.916 | 0.922 | 0.929 | 0.935 |
| 0.900 | 0.906 | 0.912 | 0.918 | 0.924 | 0.930 |
| 0.895 | 0.901 | 0.907 | 0.913 | 0.919 | 0.926 |
| 0.891 | 0.897 | 0.903 | 0.909 | 0.915 | 0.921 |
| 0.886 | 0.892 | 0.898 | 0.904 | 0.910 | 0.916 |
| 0.881 | 0.887 | 0.893 | 0.899 | 0.905 | 0.911 |
| 0.877 | 0.883 | 0.889 | 0.895 | 0.901 | 0.907 |
| 0.872 | 0.878 | 0.884 | 0.890 | 0.896 | 0.902 |
| 0.867 | 0.873 | 0.879 | 0.885 | 0.891 | 0.897 |

The expired minute volume ( $\dot{V}_E$ ) is adjusted to standard temperature and atmospheric pressure, i.e. 0°C and 760 mmHg dry (STPD) by the relation.

$$\dot{V}_{STPD} = A \times \dot{V}_E \quad \dots (5)$$

where A is an adjustment factor which can be obtained from the *Documenta Geigy Scientific Tables* (1962), a modification of which is depicted in the Table.

For STPD conditions:

$$A = \frac{273}{273 + T} \times \frac{P - P_{H_2O}}{760} \quad \dots (6)$$

where T = ambient temperature (°C)  
 P = ambient barometric pressure (mmHg)  
 $P_{H_2O}$  = water vapour pressure at temperature, T (mmHg).

From (4) and (5) we have corrected  $\dot{V}O_2$

$$= A [(0.265 \times \dot{V}_E) - (1.265 \times \dot{V}_E \times F_{E O_2}) - (0.265 \times \dot{V}_E \times F_{E CO_2})] \quad \dots (7)$$

Equation (7) was used to calculate the oxygen consumption depicted in the nomogram in Fig. 1.

## Application

With a sharp point of a calliper, mark the fractional concentration of expired  $CO_2$  on the line  $CO_2$  and fractional concentration of expired  $O_2$  on line  $O_2$ . Join the two points with a straight line to cross the unscaled line x. By joining the point so obtained on line x and the expired volume ( $\dot{V}_E$ ) on line  $\dot{V}_E$  a straight line may be extended to meet line  $\dot{V}O_2$  yielding the oxygen consumption (l/min).

The corrected oxygen consumption ( $\dot{V}O_2$  corr) may then be obtained by joining the point on line  $\dot{V}O_2$  to the adjustment factor A on line A with a straight line and extending it to meet the line  $\dot{V}O_2$  corr (example A). If the oxygen consumption is expected to exceed 0.8 l/min, use half the value of  $\dot{V}_E$  and double the resultant oxygen consumption (example B). In strenuous exercise it may be necessary to use 1/10th the value of  $\dot{V}_E$  and multiply the resultant  $O_2$  consumption by 10.

## Examples (Fig. 2)

(A)  $F_{E CO_2} = 0.05$ ,  $F_{E O_2} = 0.18$ ,  $\dot{V}_E = 5$  l/min,  
 A = 0.9

Then  $\dot{V}O_2 = 0.120$  l/min,  $\dot{V}O_2$  corr = 0.108 l/min by nomography and calculation.

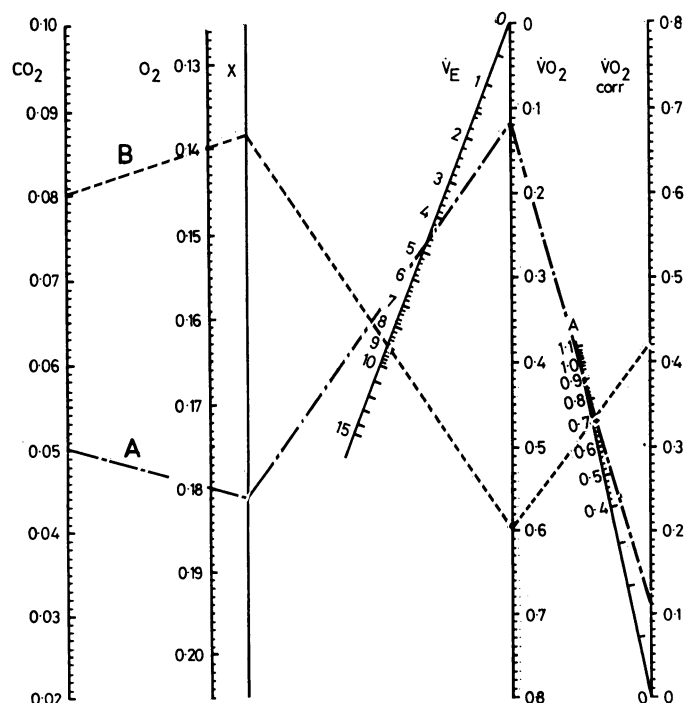


Fig. 2 Illustrated use of nomogram using two examples as described in the text (A and B).

- (B)  $F_{E\text{ CO}_2} = 0.08$ ,  $F_{E\text{ O}_2} = 0.14$ ,  $\dot{V}_E = 18$  l/min,  
     $A = 0.7$   
    Then  $\dot{V}_{\text{O}_2}$  corr = 0.420 l/min from nomogram  
    using  $\dot{V}_E = 9$  l/min,  $F_{E\text{ CO}_2} = 0.08$ ,  $F_{E\text{ O}_2} =$   
    0.14,  $A = 0.7$ .  
    Hence corrected  $\dot{V}_{\text{O}_2} = 2 \times 0.420$  or 0.840 l/min  
    when  $\dot{V}_E = 18$ .

**Reference**

*Documenta Geigy Scientific Tables* (1962). 6th ed., pp. 300-309  
ed K. Diem. Geigy Pharmaceuticals, Ardsley, New York.

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